



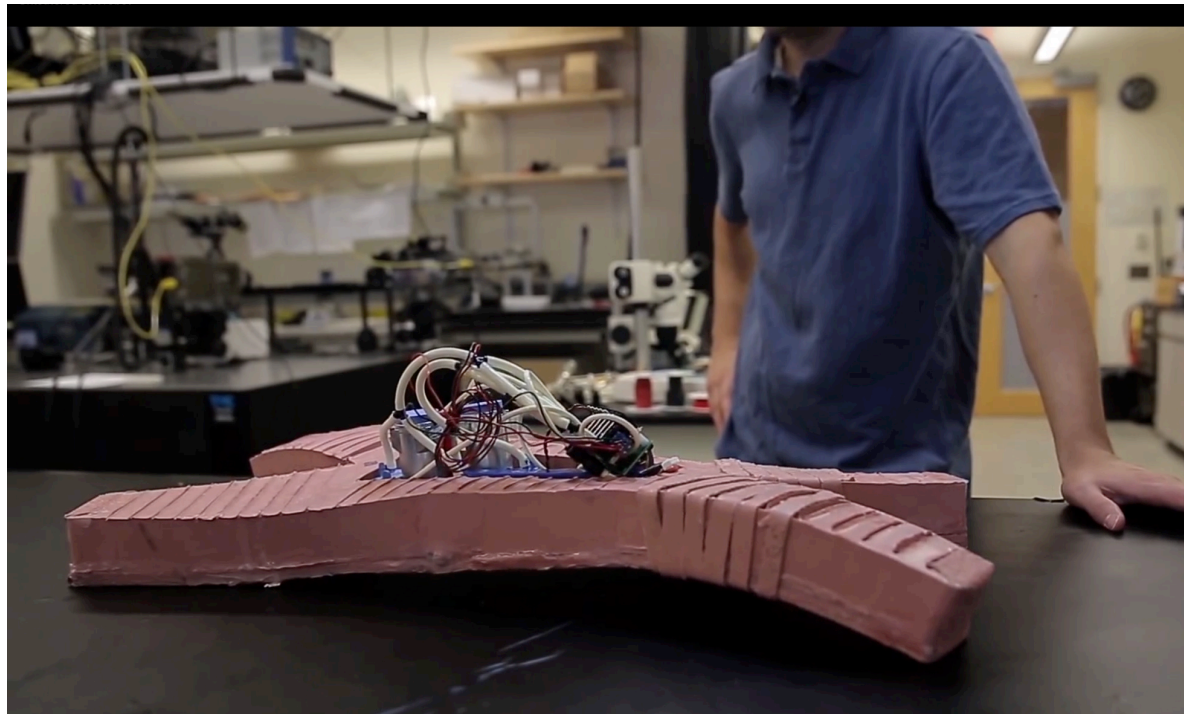
E160 – Lecture 4

Autonomous Robot Navigation

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Semester: Spring 2016



Soft Robotics

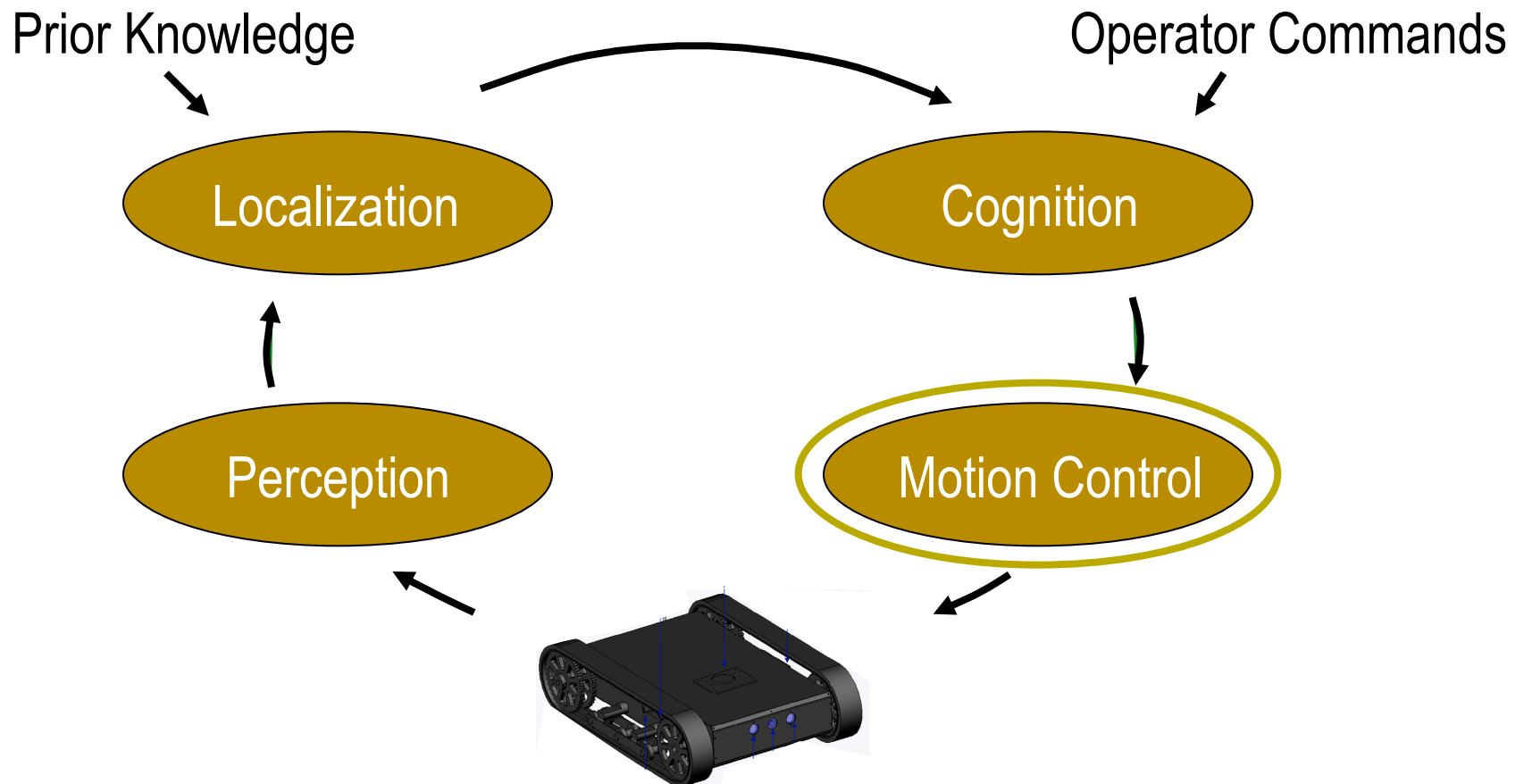


https://www.youtube.com/watch?v=_OJrwCP24cl



Control Structures

Planning Based Control





Point Tracking

1. P Control
2. Linear Systems
3. Motion Control
4. Reachable Space



P Control

- Proportional Feedback Control – P Control
 - Uses the error between the desired and measured state to determine the control signal.



P Control

- If $x_{desired}$ is the desired state, and x is the actual state, we define the error as:

$$e = x_{desired} - x$$



P Control

- The control signal u is calculated as

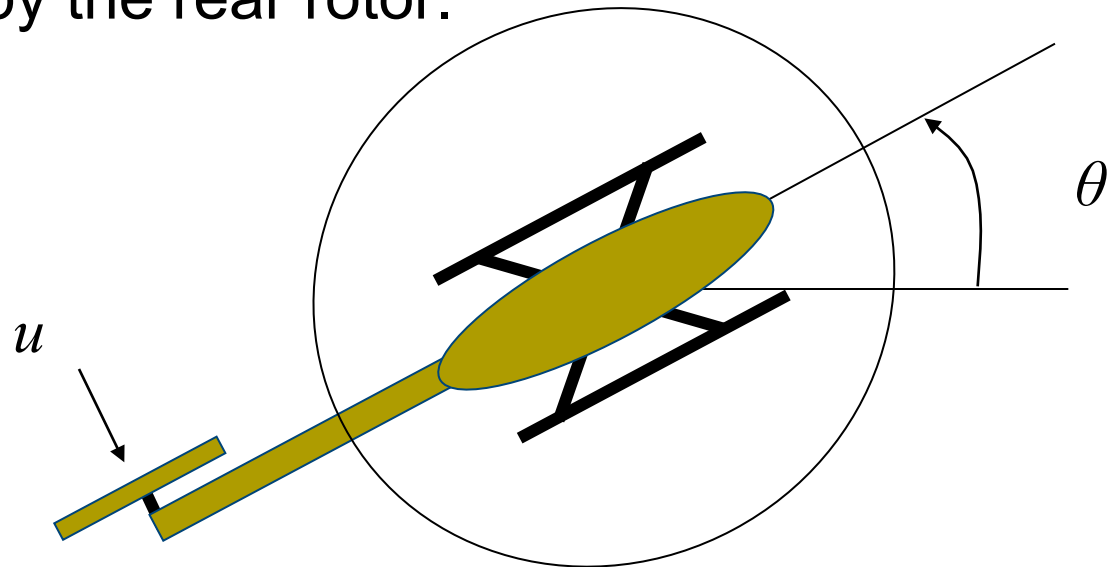
$$u = K_P e$$

where K_P is called the proportional gain.



P Control

- Example:
 - Consider the orientation control of an autonomous helicopter. Assume the orientation is completely controlled by the rear rotor.





P Control

- Example cont':
 - The control signal u is calculated as

$$u = K_P(\theta_{desired} - \theta)$$

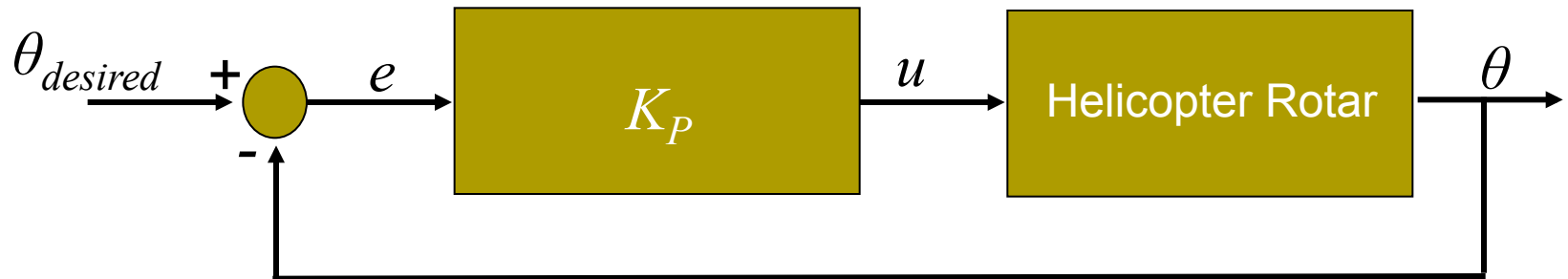
- Notes:
 - If $\theta_{desired} = \theta$, the control signal is 0 .
 - If $\theta_{desired} < \theta$, the control signal is negative, resulting in a decrease in θ .
 - If $\theta_{desired} > \theta$, the control signal is positive, resulting in an increase in θ .
 - The magnitude of the increase/decrease depends on K_p



P Control

- Block Diagram:

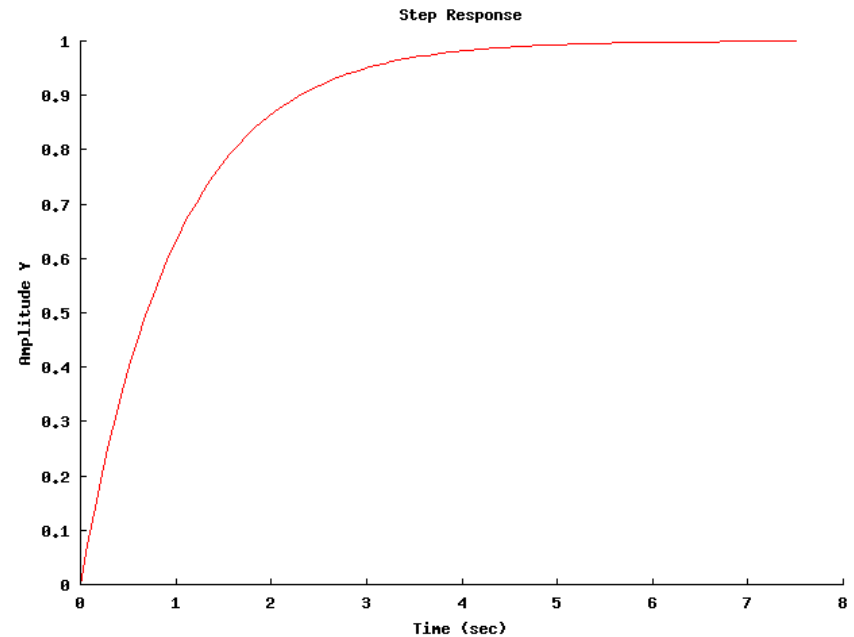
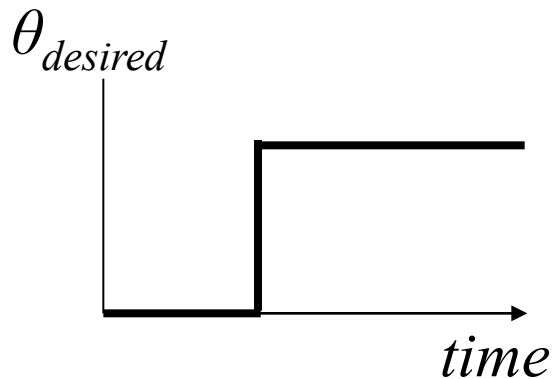
$$u = K_P(\theta_{desired} - \theta)$$





P Control

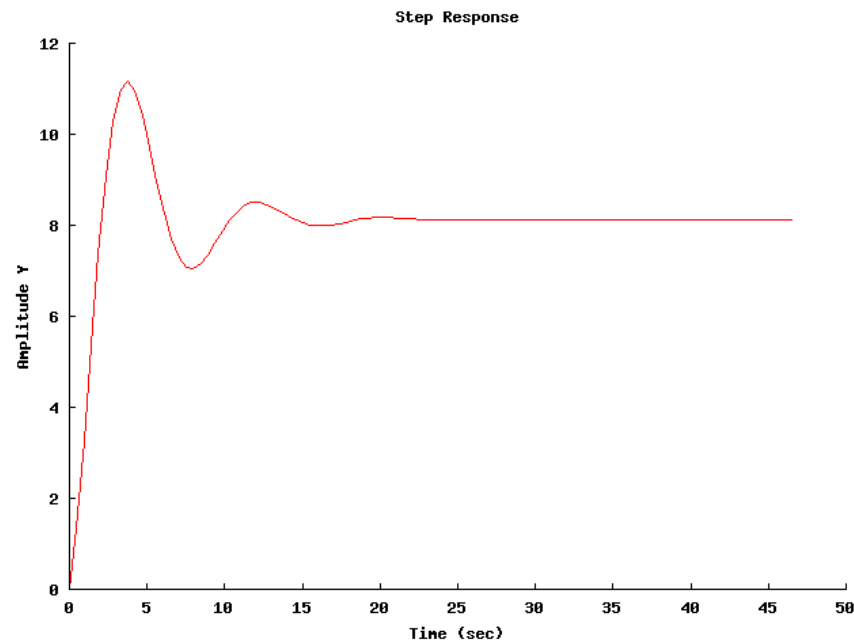
- Time Domain Response of step response
 - Step from $\theta_{desired} = 0$ to $\theta_{desired} = 1$.





P Control

- Time Domain Response:
 - Step from $\theta_{desired} = 0$ to $\theta_{desired} = 8$.
 - Different dynamics in this example... overshoot!





Point Tracking

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Linear Systems

- Recall that the forward kinematics are a linear differential equation.
- We will use this equation to help develop a motion controller for point tracking
- We start by observing how the state x behaves if it obeys the following equation:

$$\dot{x} = dx/dt = ax$$

where a is a constant



Linear Systems

- It should be obvious that the solution to the equation

$$\dot{x} = ax$$

is

$$x(t) = x_0 \exp(at)$$

where

x_0 is the initial state



Linear Systems

- To confirm this solution, substitute into the original equation:

$$\dot{x} = ax$$

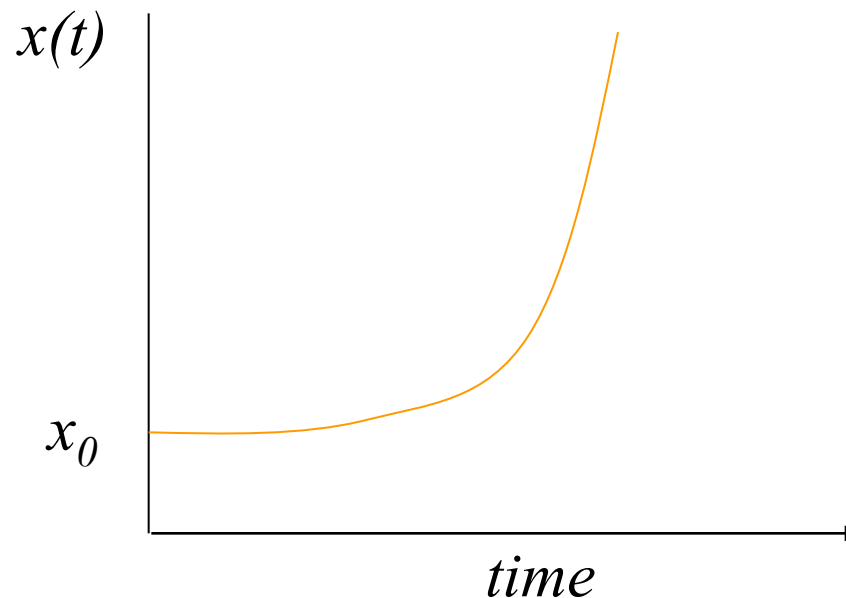
$$d[x_0 \exp(at)]/dt = a[x_0 \exp(at)]$$

$$ax_0 \exp(at) = ax_0 \exp(at)$$



Linear Systems

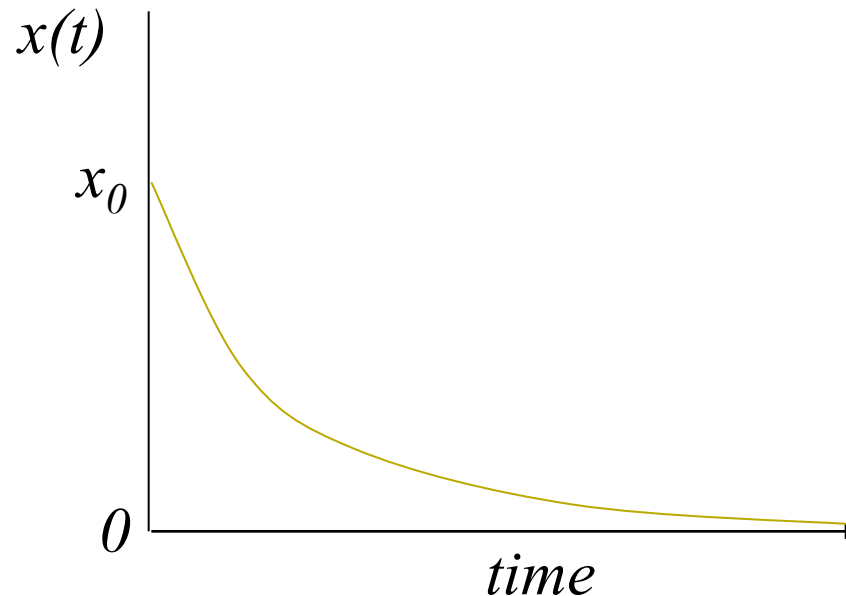
- To view how the state x behaves over time, we can plot out $x = x_0 \exp(at)$, assuming a is positive:





Linear Systems

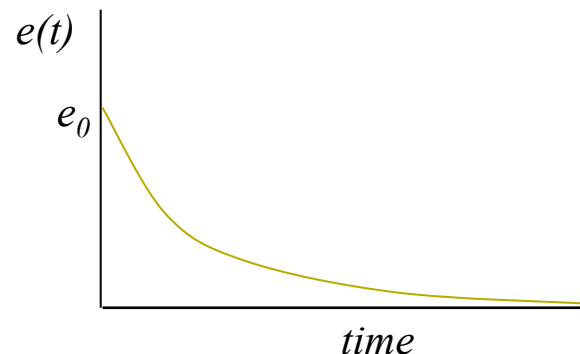
- If a is negative and we can plot out $x = x_0 \exp(at)$, we get much different results:





Linear Systems

- This exponential decay informs us that the state x decays to zero over time.
 - We say this system is “STABLE”.
 - We use this property in control theory to drive states down to zero (e.g. if $e = x_{desired} - x$, drive e to 0).





Linear Systems

- The above example was a one dimensional linear system (i.e. single state x).
- Our system is a multi-dimensional system (i.e. 3 states x, y, θ).
- We need to describe the system with matrices:

$$\dot{\mathbf{x}} = A\mathbf{x}$$

where A is a matrix such that $A \in R^{n \times n}$

\mathbf{x} is a vector such that $\mathbf{x} \in R^{1 \times n}$



Linear Systems

- The eigen values of A , represented by λ_i , are coefficients that satisfy the equation:

$$A\mathbf{x}_i = \lambda_i \mathbf{x}_i$$

for particular states called \mathbf{x}_i , called the eigen vectors.

- A solution to the system can be written as the combination of eigen vectors:

$$\mathbf{x}(t) = \mathbf{x}_1 e^{\lambda_1 t} + \mathbf{x}_2 e^{\lambda_2 t} + \dots + \mathbf{x}_n e^{\lambda_n t}$$



Linear Systems

- In this case, the system

$$\dot{\mathbf{x}} = A\mathbf{x}$$

is said to be stable if the eigen-values of A are less than 0 .



Linear Systems

- We solve for eigen values by noting:

$$(A - \lambda I)\mathbf{x} = 0$$

- For this to hold true,

$$\det (A - \lambda I) = 0$$



Linear Systems

- Example:

$$A = \begin{bmatrix} 3 & 6 \\ 1 & 4 \end{bmatrix}.$$

$$A - \lambda I = \begin{bmatrix} 3 - \lambda & 6 \\ 1 & 4 - \lambda \end{bmatrix}$$

$$\det(A - \lambda I) = (3 - \lambda)(4 - \lambda) - 6$$

$$= \lambda^2 - 7\lambda + 6$$

$$= (\lambda - 6)(\lambda - 1)$$

Therefore $\lambda_1 = 6$, $\lambda_2 = 1$

The system is not stable!



Linear Systems

- Summary:
 - If our robot behaves like a system of the form $\dot{e} = Ae$, where the eigen values of A are negative and e represents the difference between desired and actual states, the system will move to our desired state!



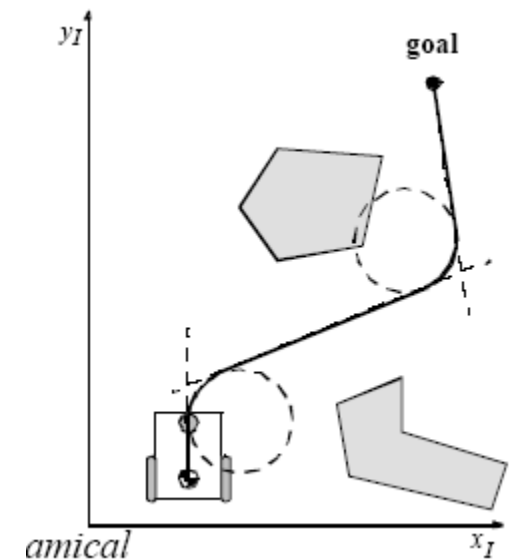
Point Tracking

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Motion Control

- Goal is to follow a trajectory from an initial state to some desired goal location.
- Several approaches
 - Could construct a global trajectory first, then track **points** on the trajectory locally





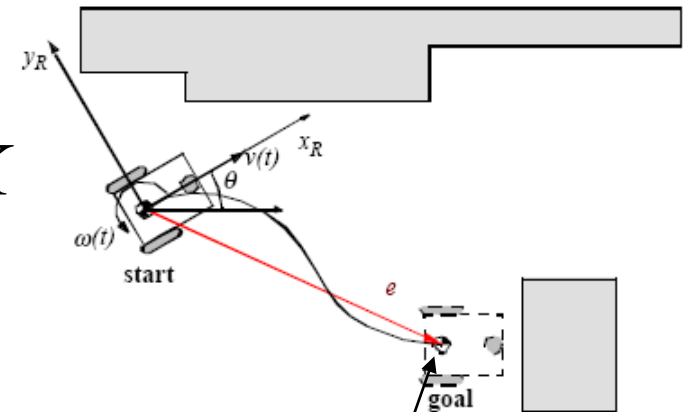
Motion Control

- If we define the error to be in the robot frame:

$$e(t) = [x \ y \ \theta]^T$$

- Goal is to find gain matrix K such that control of $v(t)$ and $w(t)$ will drive the error $e(t)$ to zero.

$$\begin{bmatrix} v(t) \\ w(t) \end{bmatrix} = Ke(t)$$



Assume goal is at $[0 \ 0 \ 0]$



Motion Control

- Recall our forward kinematics

$$\begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{pmatrix} = \begin{pmatrix} \cos\theta & 0 \\ \sin\theta & 0 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} v \\ w \end{pmatrix}$$



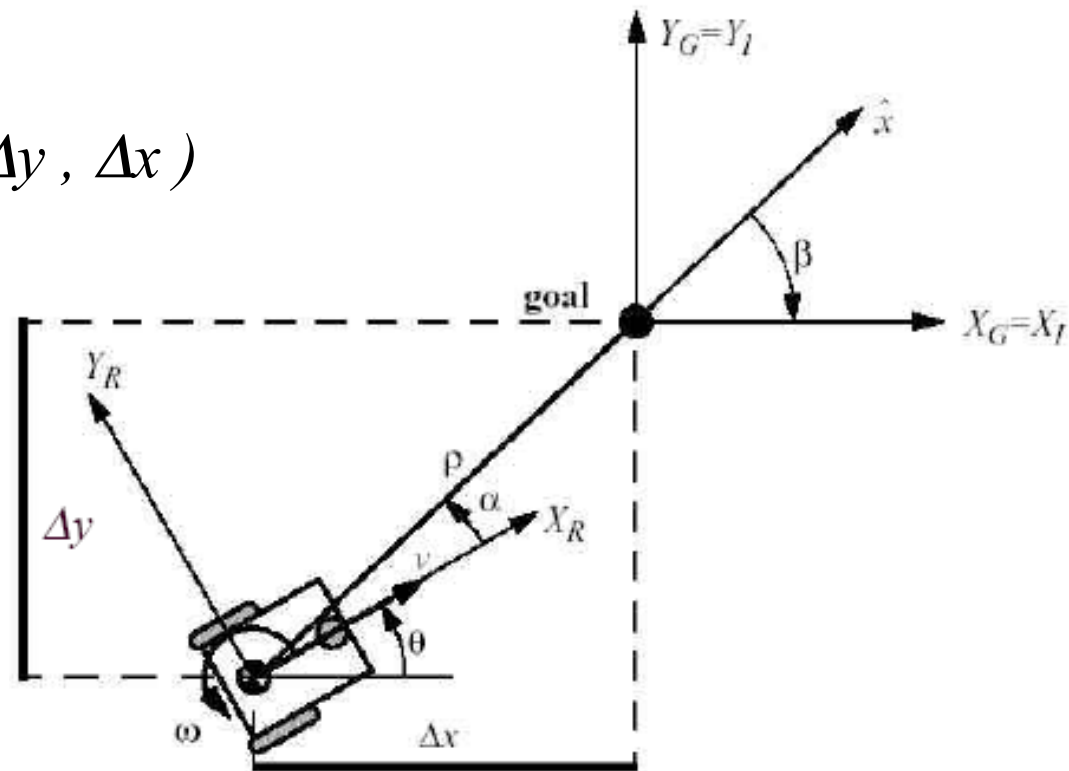
Motion Control

- We use the coordinate transformation

$$\rho = \sqrt{\Delta x^2 + \Delta y^2}$$

$$\alpha = -\theta + \text{atan2}(\Delta y, \Delta x)$$

$$\beta = -\theta - \alpha$$





Motion Control

- Now we define the problem as driving the robot to goal

$$\begin{pmatrix} \rho \\ \alpha \\ \beta \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$



Motion Control

- We know this will happen if the dynamics of the system obey

$$\begin{pmatrix} \dot{\rho} \\ \dot{\alpha} \\ \dot{\beta} \end{pmatrix} = A \begin{pmatrix} \rho \\ \alpha \\ \beta \end{pmatrix}$$

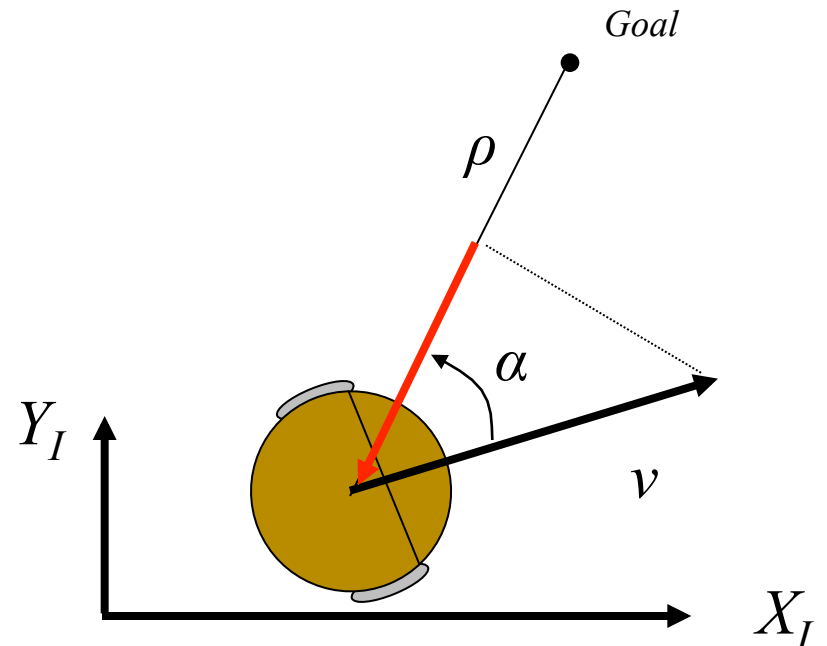
Where A is a 3×3 matrix with eigen values less than 0 .



Motion Control

- Using the coordinate transformation, calculate the new kinematics:

$$\begin{aligned}\dot{\rho} &= \text{projection of } v \text{ on } \rho \\ &= -v \cos(\alpha)\end{aligned}$$





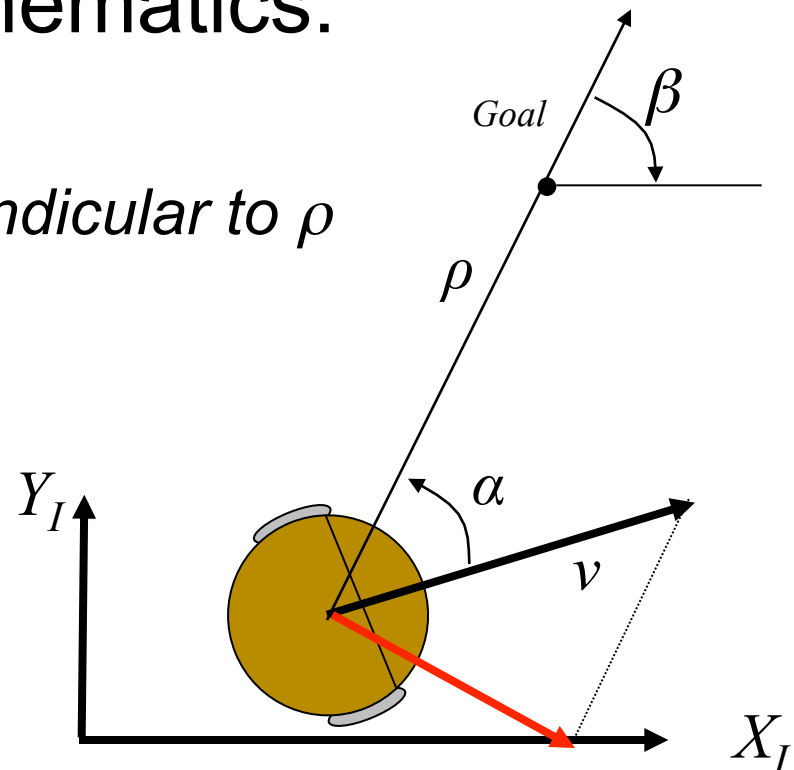
Motion Control

- Using the coordinate transformation, calculate the new kinematics:

$\rho \dot{\beta} = \text{projection of } v \text{ perpendicular to } \rho$

$$= -v \sin(\alpha)$$

$$\dot{\beta} = -v \sin(\alpha) / \rho$$



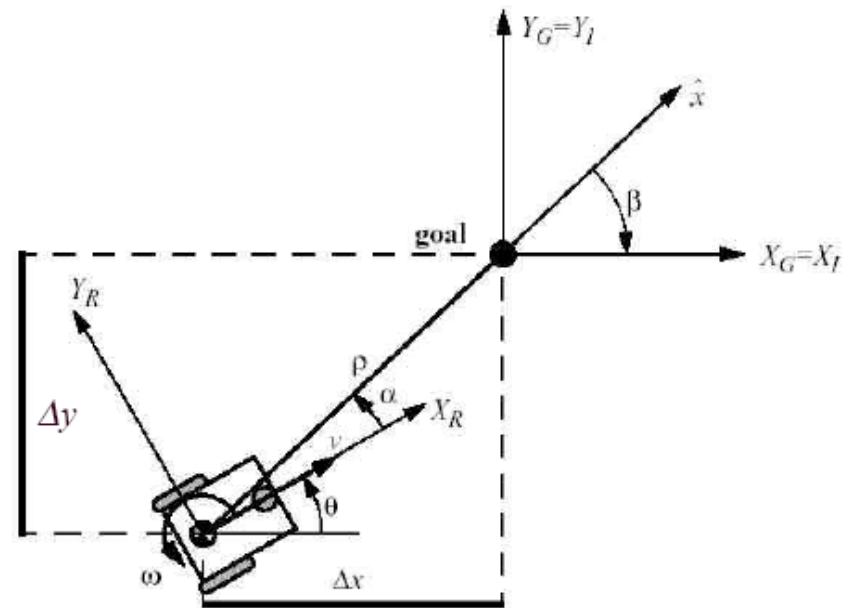
Motion Control

- Using the coordinate transformation, calculate the new kinematics:

$$\alpha = -\beta - \theta$$

$$\dot{\alpha} = -\dot{\beta} - \dot{\theta}$$

$$\dot{\alpha} = v \sin(\alpha) / \rho - w$$





Motion Control

- In matrix form:

$$\begin{pmatrix} \dot{\rho} \\ \dot{\alpha} \\ \dot{\beta} \end{pmatrix} = \begin{pmatrix} -\cos\alpha & 0 \\ \sin\alpha / \rho & -1 \\ -\sin\alpha / \rho & 0 \end{pmatrix} \begin{pmatrix} v \\ w \end{pmatrix} \quad \text{for } \alpha \text{ within } (-\pi/2, \pi/2]$$



Motion Control

- Let's try the control law:

$$v = k_{\rho}\rho \quad w = k_{\alpha}\alpha + k_{\beta}\beta$$

- Note that this is a form of P control, and if ρ , α , β all go to zero, then v and w will go to zero.



Motion Control

- To analyze controller, substitute control law into kinematics and linearize:
 - For small x , $\cos(x) \approx 1$ and $\sin(x) \approx x$

- This is in the form...

$$\dot{e} = A e$$



Motion Control

- Check for stability:
 - Take the determinant of A and solving for eigen values leads to:

$$(\lambda + k_\rho) (\lambda^2 + \lambda (k_\alpha - k_\rho) - k_\rho k_\beta) = 0$$

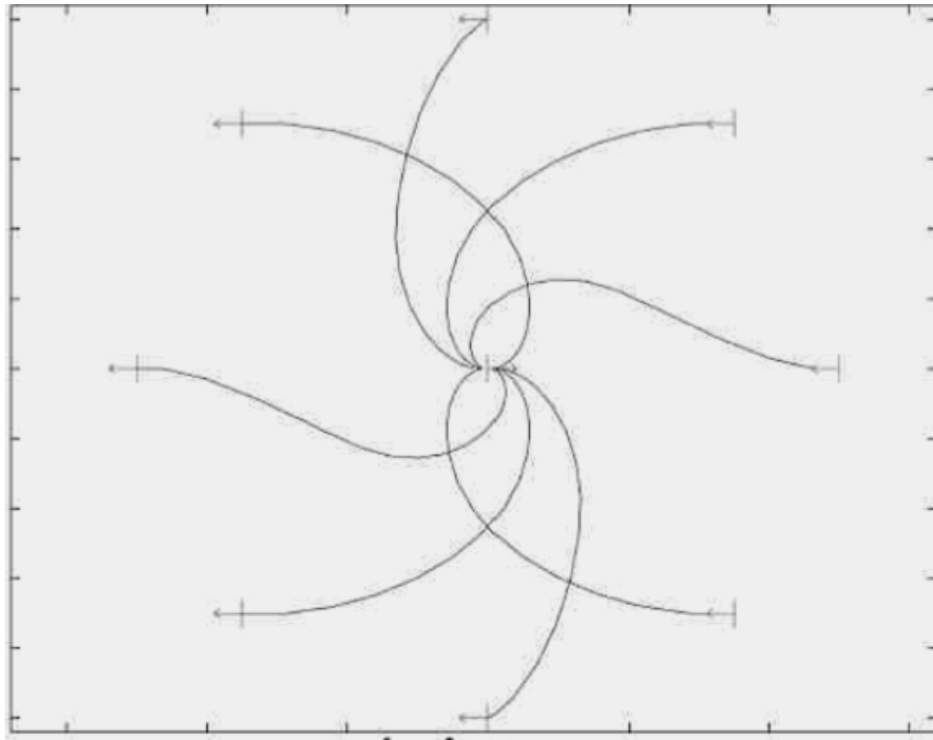
- Thus the system will be stable if:

$$k_\rho > 0 \quad k_\beta < 0 \quad k_\alpha - k_\rho > 0$$



Motion Control

- Testing this control law with many different start points:





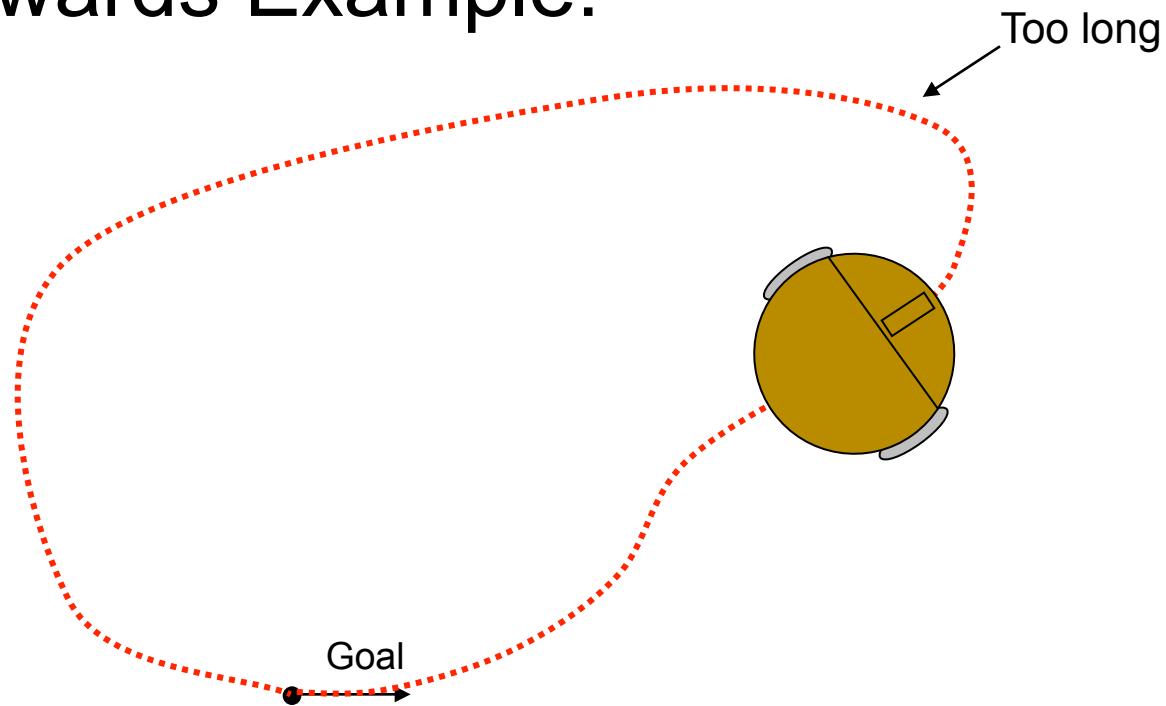
Motion Control

- The derived control law works well if $\alpha \in [-\pi/2, \pi/2]$
- For other cases where $abs(\alpha) > \pi/2$, we must modify the controller. So that the robot will move backwards to the desired position when required



Motion Control

- Backwards Example:





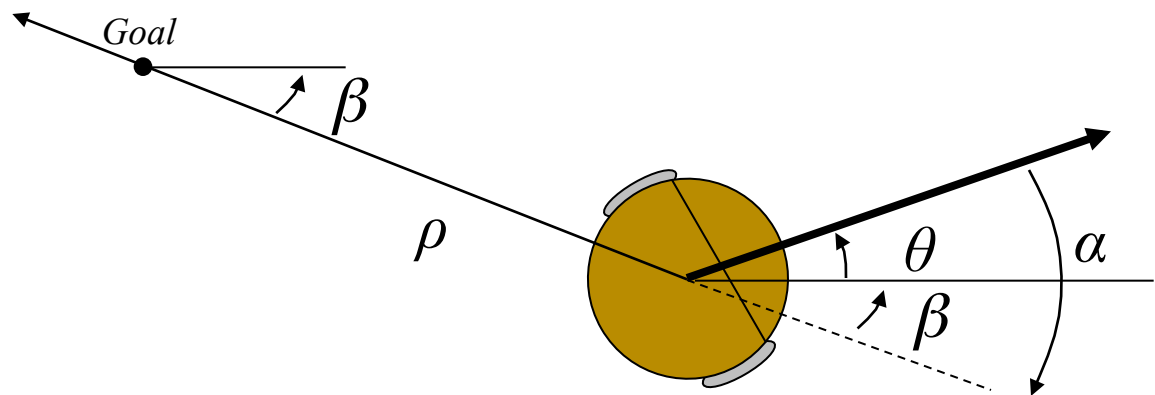
Motion Control

- Backwards Method:

$$\rho = \sqrt{\Delta x^2 + \Delta y^2}$$

$$\alpha = -\theta + \text{atan2}(-\Delta y, -\Delta x)$$

$$\beta = -\theta - \alpha$$





Motion Control

- Backwards Method Summary:
 - If $\alpha \in [-\pi/2, \pi/2]$
 - Use regular transform to polar coordinates
 - Use control law: $v = k_\rho \rho \quad w = k_\alpha \alpha + k_\beta \beta$
 - Else
 - Redefine α as shown in backwards method
 - Use control law: $v = -k_\rho \rho \quad w = k_\alpha \alpha + k_\beta \beta$



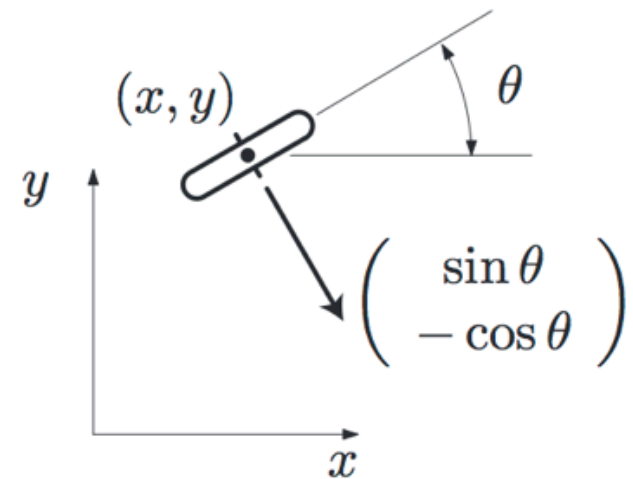
Point Tracking

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Reachable Space

- Kinematic Constraints
 - One can calculate constraints on each individual wheel, then combine for constraints on entire robot.



<http://www.cs.cmu.edu/afs/cs/academic/class/16741-s07/www/lecture5.pdf>



Reachable Space

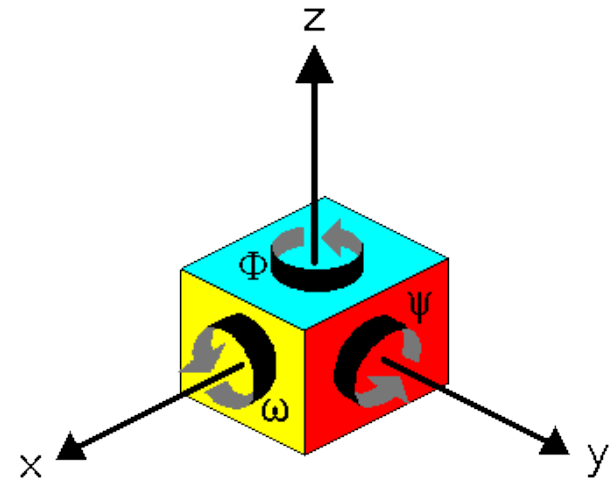
- Two main constraints:
 1. Rolling Constraint: no slipping!
 2. Sliding Constraint: no lateral movement!





Reachable Space

- Degrees of Freedom:
 - Def' n: The number of coordinates that it takes to uniquely specify the state of a system.
 - In 3D, there are 6 degrees of freedom associated to the movement of a rigid body: 3 for its position, and 3 for its orientation.

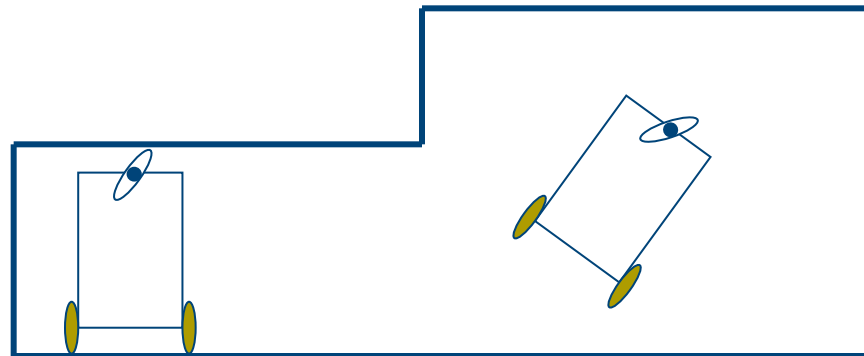


B J Stone, Univ. of Western Australia



Reachable Space

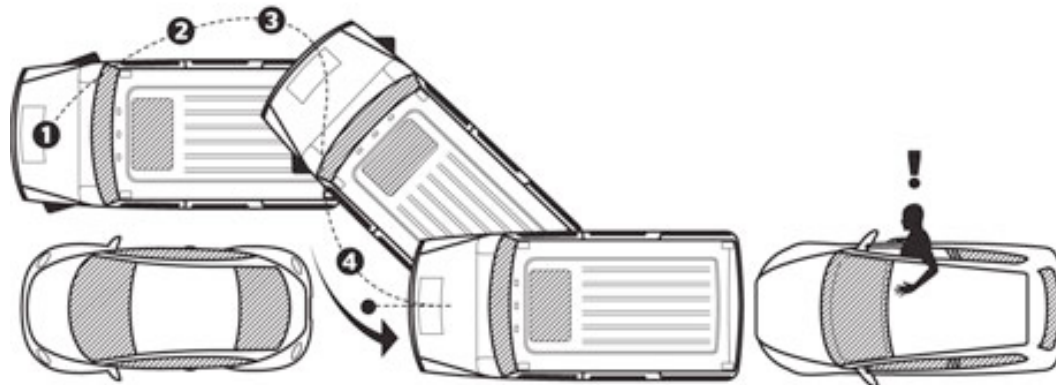
- Configurations in the Workspace
 - A robot's workspace is defined by the Degrees Of Freedom of the robot state.
 - Not all robot configurations within the workspace are reachable





Reachable Space

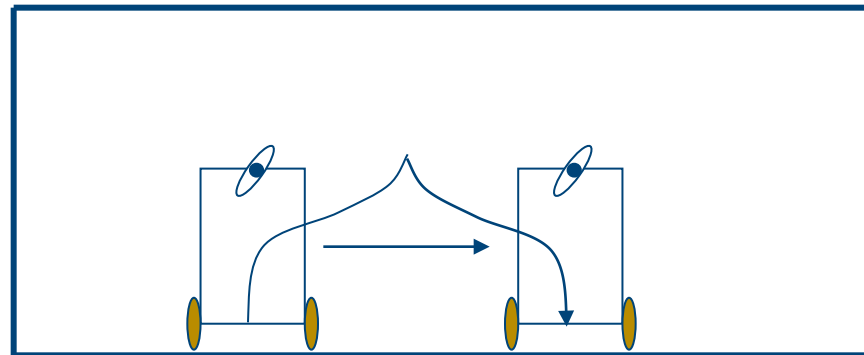
- NonHolonomic Robots
 - A nonholonomic constraint is one that is not integrable.





Reachable Space

- Paths in the Workspace
 - Path's in the workspace are limited, especially if the robot is nonholonomic





Reachable Space

- Trajectories in the Workspace
 - A trajectory is a path parameterized by time.
 - Admissible paths don't always lead to admissible trajectories.

