



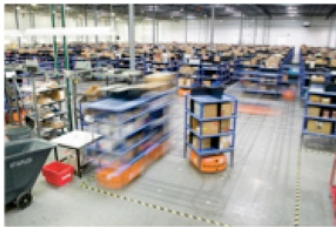
ARW – Lecture 01

Odometry Kinematics

Instructor: Chris Clark

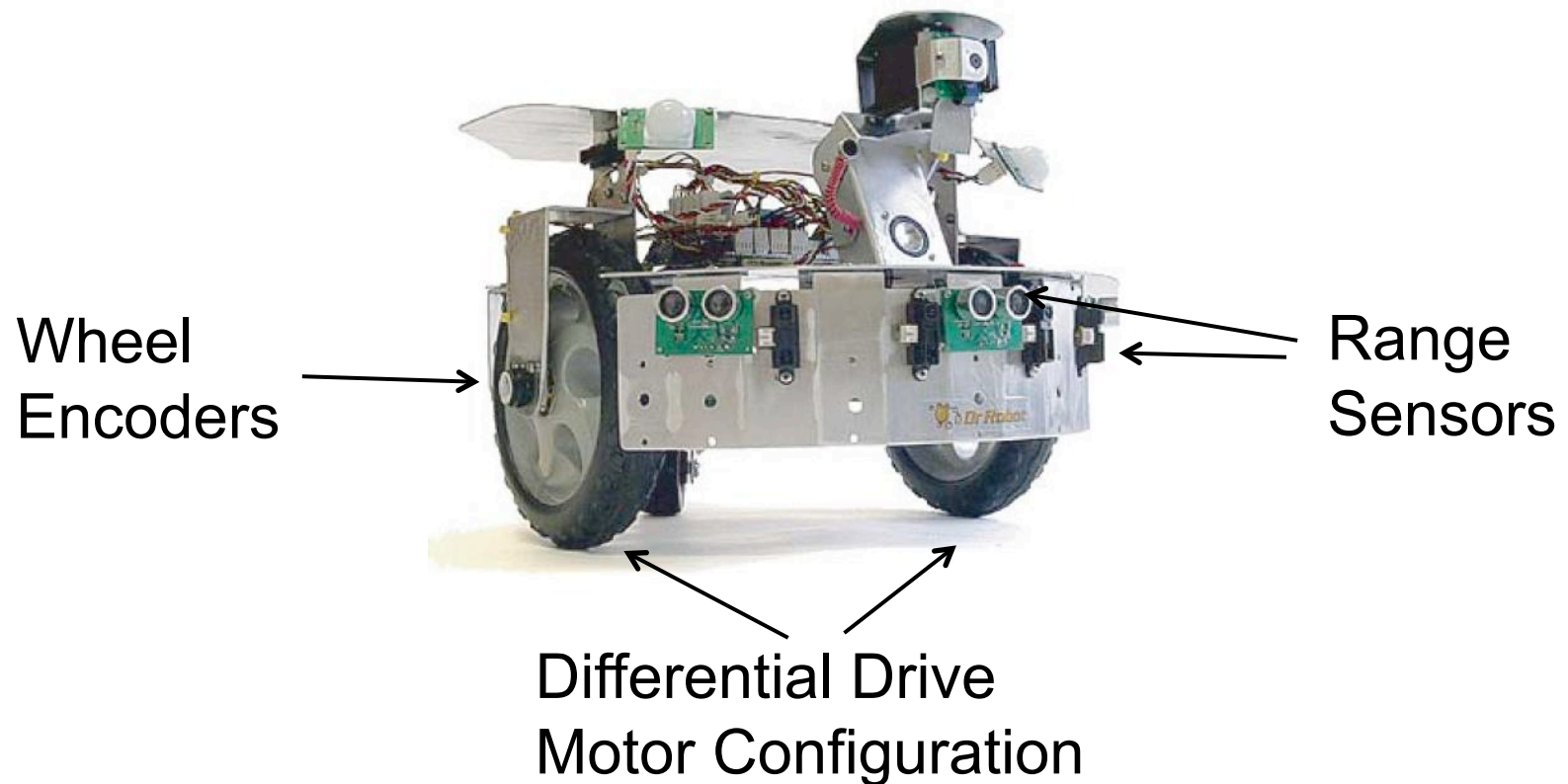
Semester: Summer 2016

Introduction





Different Bots

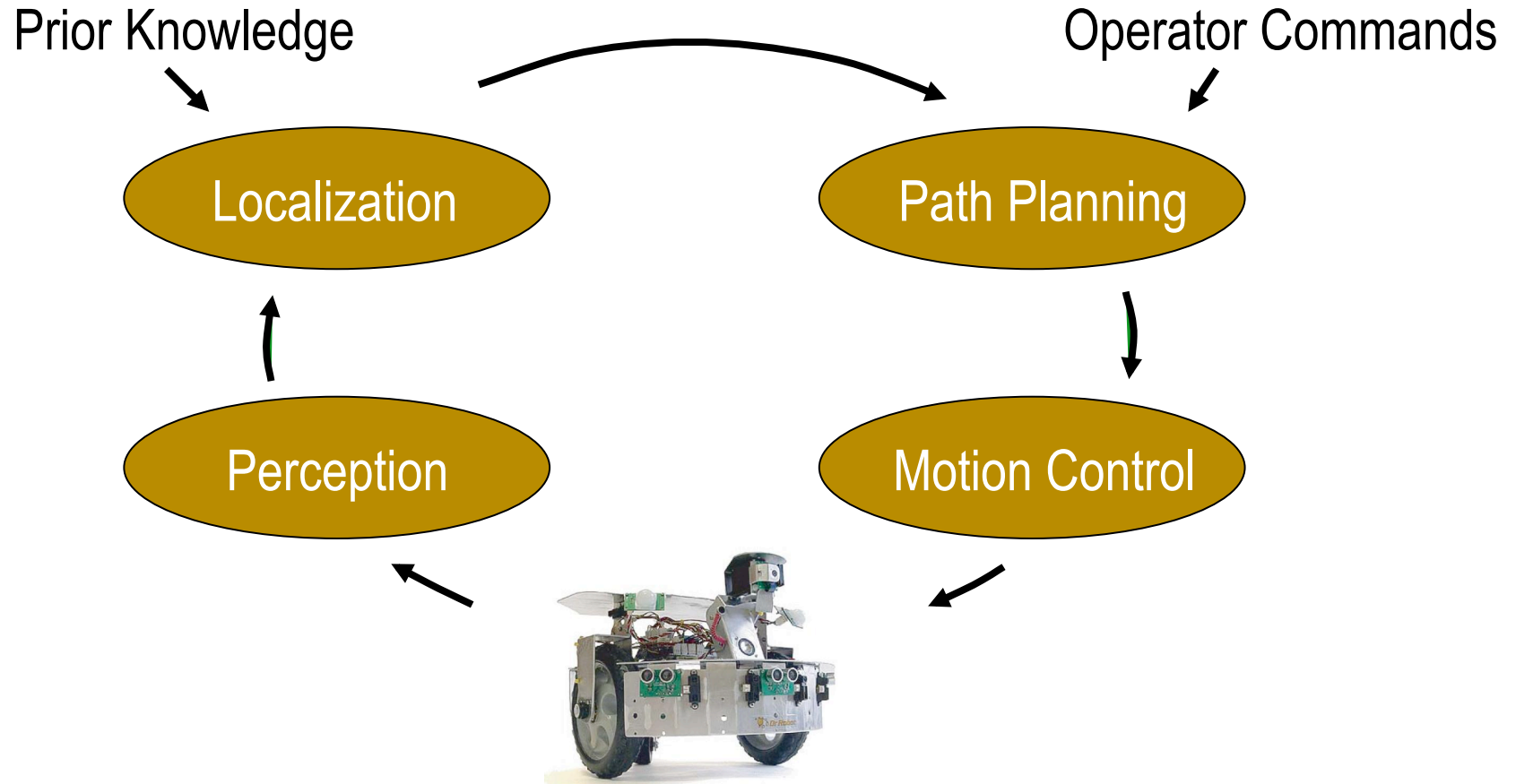


Different Bots



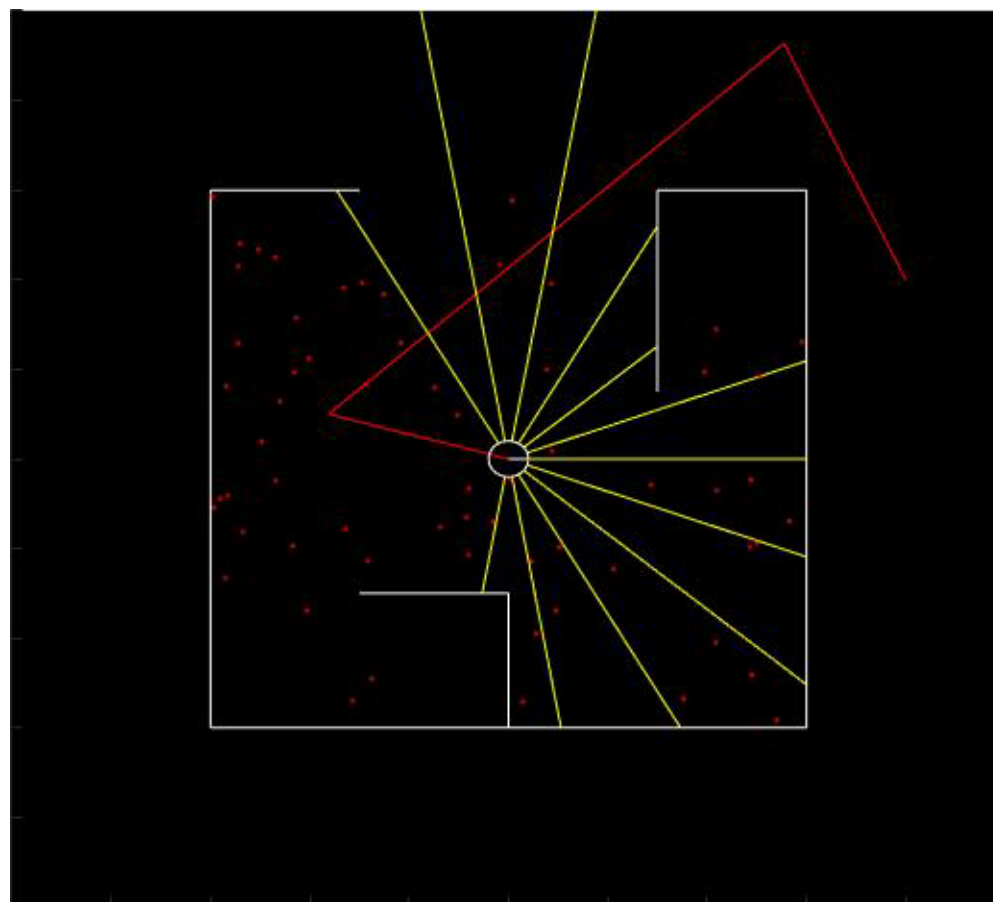


Planning Based Control





ARW Goals





Odometry Kinematics

- Lecture Goal
 - Develop an equation that maps the previous robot state and wheel encoder measurements to the new robot state.

$$X_t = f(X_{t-1}, U_{t-1})$$



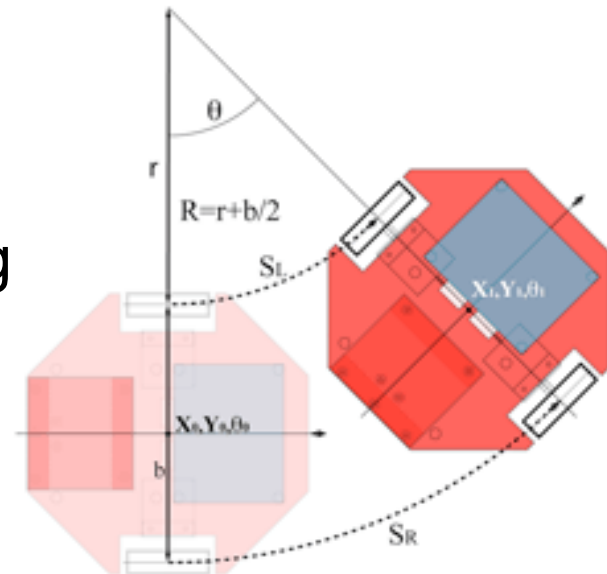
Odometry Kinematics

1. Odometry & Dead Reckoning
2. Modeling motion – The X80
3. Modeling motion – An ROV
4. Odometry in your Sim



Odometry & Dead Reckoning

- Odometry
 - Use wheel sensors to update position
- Dead Reckoning
 - Use wheel sensors and heading sensor to update position
- Straight forward to implement
- Errors are integrated, unbounded



<http://www.guiott.com>



Odometry & Dead Reckoning

- Odometry Error Sources?



Odometry & Dead Reckoning

- Odometry Error Sources?
 - Limited **resolution** during integration
 - Unequal **wheel diameter**
 - Variation in the **contact** point of the wheel
 - Unequal **floor** contact and variable friction can lead to slipping



Odometry & Dead Reckoning

- Odometry Error Sources?





Odometry & Dead Reckoning

- Odometry Errors
 - **Deterministic** errors can be eliminated through proper calibration
 - **Non-deterministic** errors have to be described by error models and will always lead to uncertain position estimate.



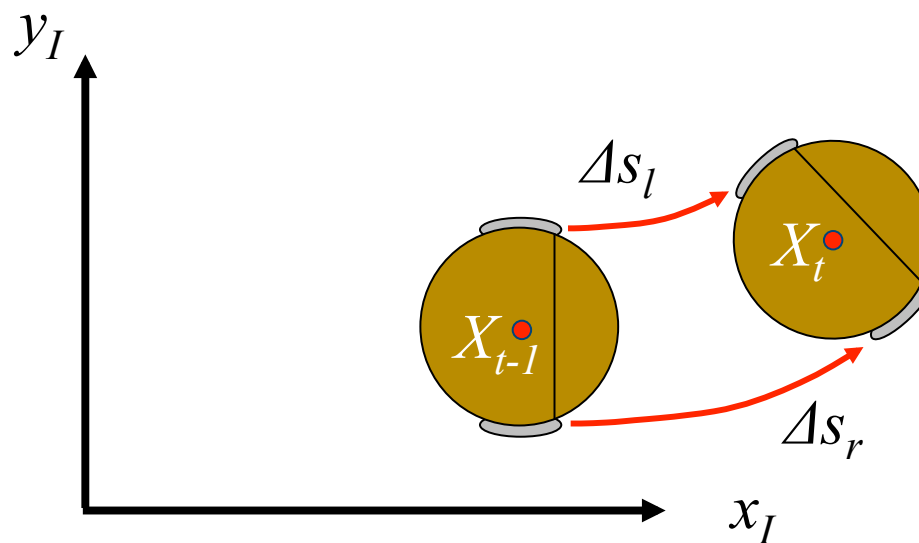
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Modeling Motion

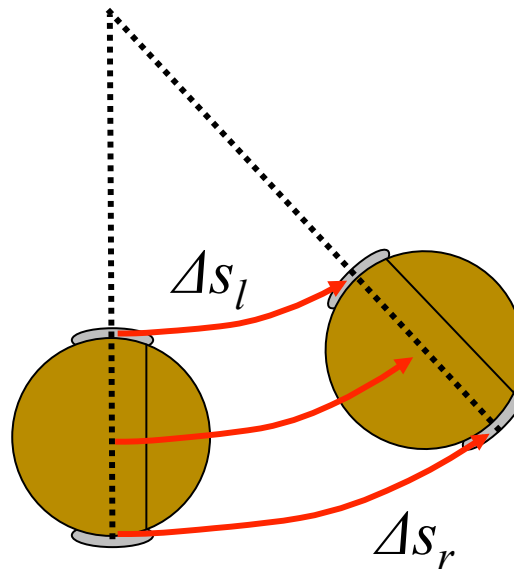
- If a robot starts from a position X_{t-1} , and the right and left wheels move respective distances Δs_r and Δs_l , what is the resulting new position X_t ?





Modeling Motion

- To start, let's model the change in angle $\Delta\theta$ and distance travelled Δs by the robot.
 - Assume the robot is travelling on a circular arc of constant radius.





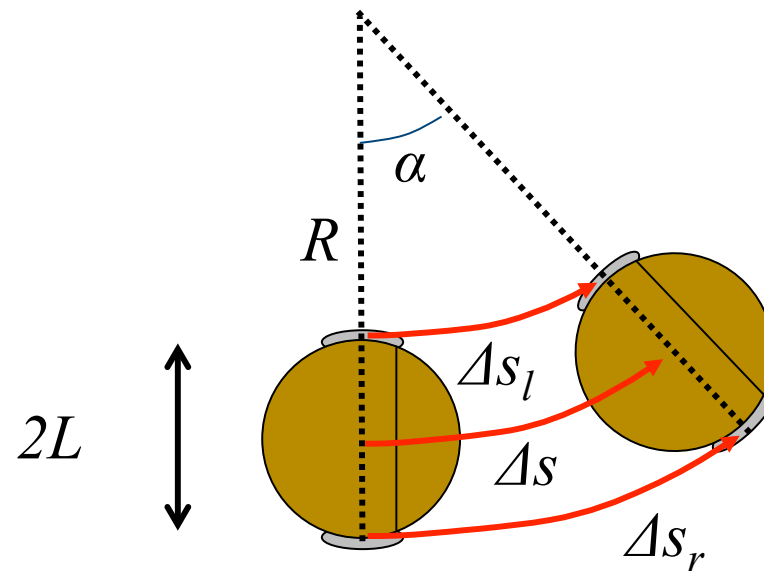
Modeling Motion

- Begin by noting the following holds for circular arcs:

$$\Delta s_l = R\alpha$$

$$\Delta s_r = (R+2L)\alpha$$

$$\Delta s = (R+L)\alpha$$





Modeling Motion

- Now manipulate first two equations:

$$\Delta s_l = R\alpha \quad \Delta s_r = (R+2L)\alpha$$

To:

$$R\alpha = \Delta s_l$$

$$L\alpha = (\Delta s_r - R\alpha)/2$$

$$= \Delta s_r/2 - \Delta s_l/2$$



Modeling Motion

- Substitute this into last equation for Δs :

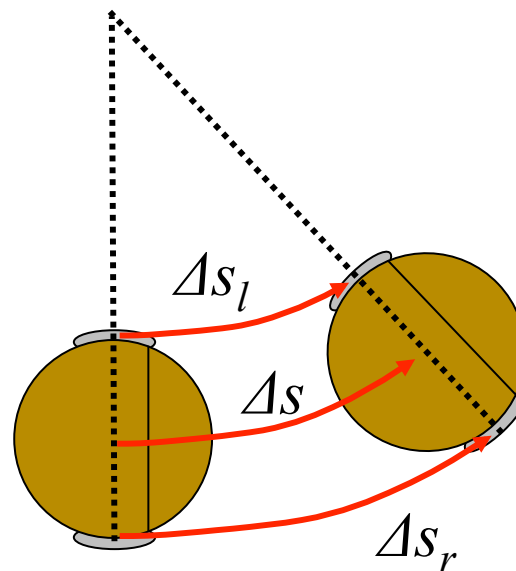
$$\begin{aligned}\Delta s &= (R+L)\alpha \\ &= R\alpha + L\alpha \\ &= \Delta s_l + \Delta s_r/2 - \Delta s_l/2 \\ &= \Delta s_l/2 + \Delta s_r/2 \\ &= \frac{\Delta s_l + \Delta s_r}{2}\end{aligned}$$



Modeling Motion

- Or, note the distance the center travelled is simply the average distance of each wheel:

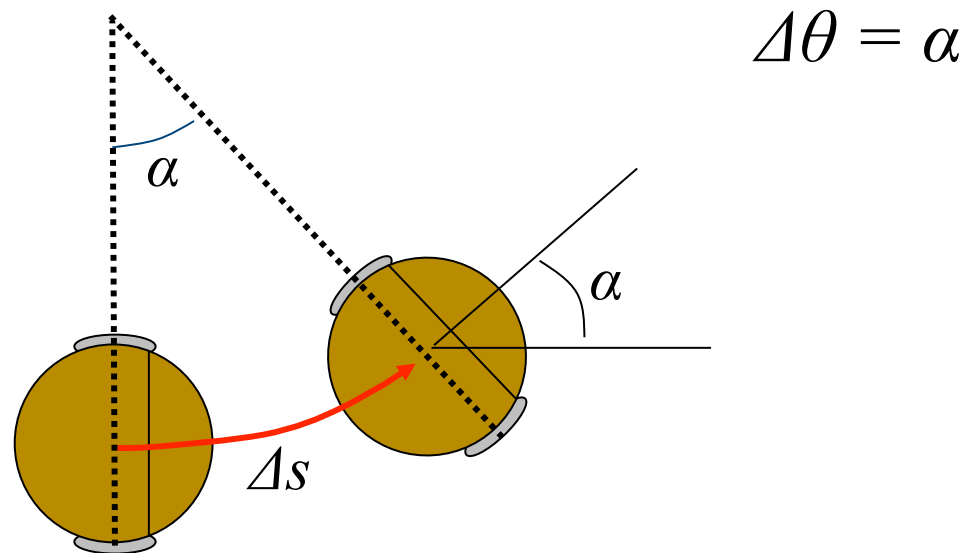
$$\Delta s = \frac{\Delta s_r + \Delta s_l}{2}$$





Modeling Motion

- To calculate the change in angle $\Delta\theta$, observe that it equals the rotation about the circular arc's center point





Modeling Motion

- So we solve for α by equating α from the first two equations:

$$\Delta s_l = R\alpha \quad \Delta s_r = (R+2L)\alpha$$

This results in:

$$\Delta s_l / R = \Delta s_r / (R+2L)$$

$$(R+2L) \Delta s_l = R \Delta s_r$$

$$2L \Delta s_l = R (\Delta s_r - \Delta s_l)$$

$$\frac{2L \Delta s_l}{(\Delta s_r - \Delta s_l)} = R$$



Modeling Motion

- Substitute R into

$$\begin{aligned}\alpha &= \Delta s_l / R \\ &= \Delta s_l (\Delta s_r - \Delta s_l) / (2L \Delta s_l) \\ &= \frac{(\Delta s_r - \Delta s_l)}{2L}\end{aligned}$$

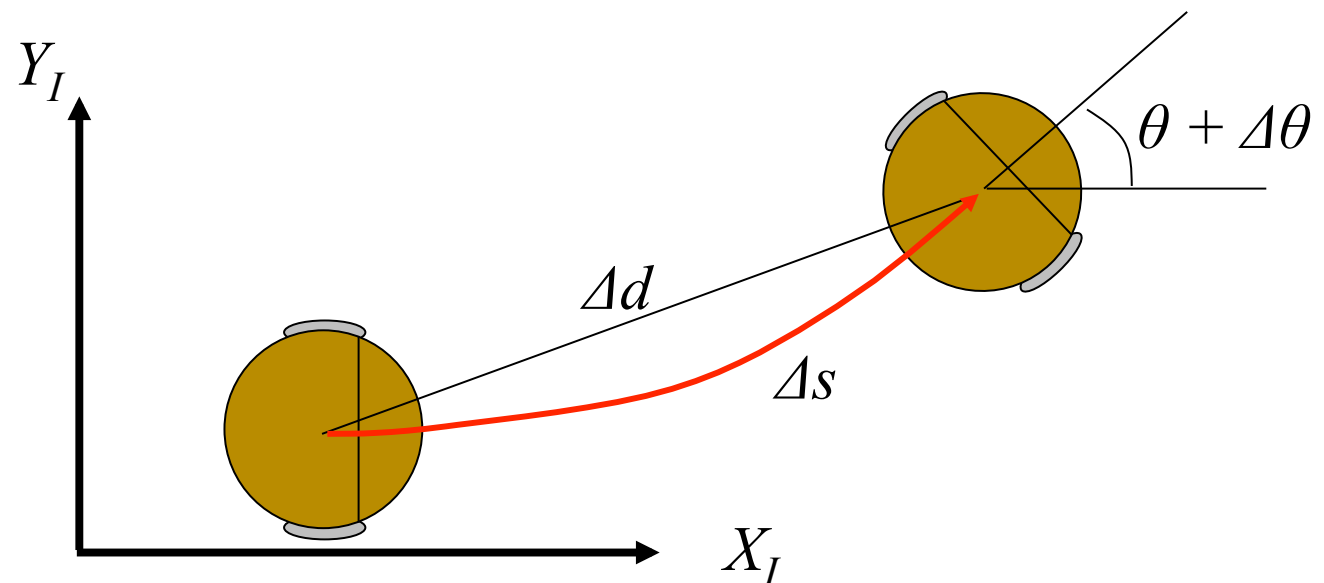
So...

$$\Delta\theta = \frac{(\Delta s_r - \Delta s_l)}{2L}$$



Modeling Motion

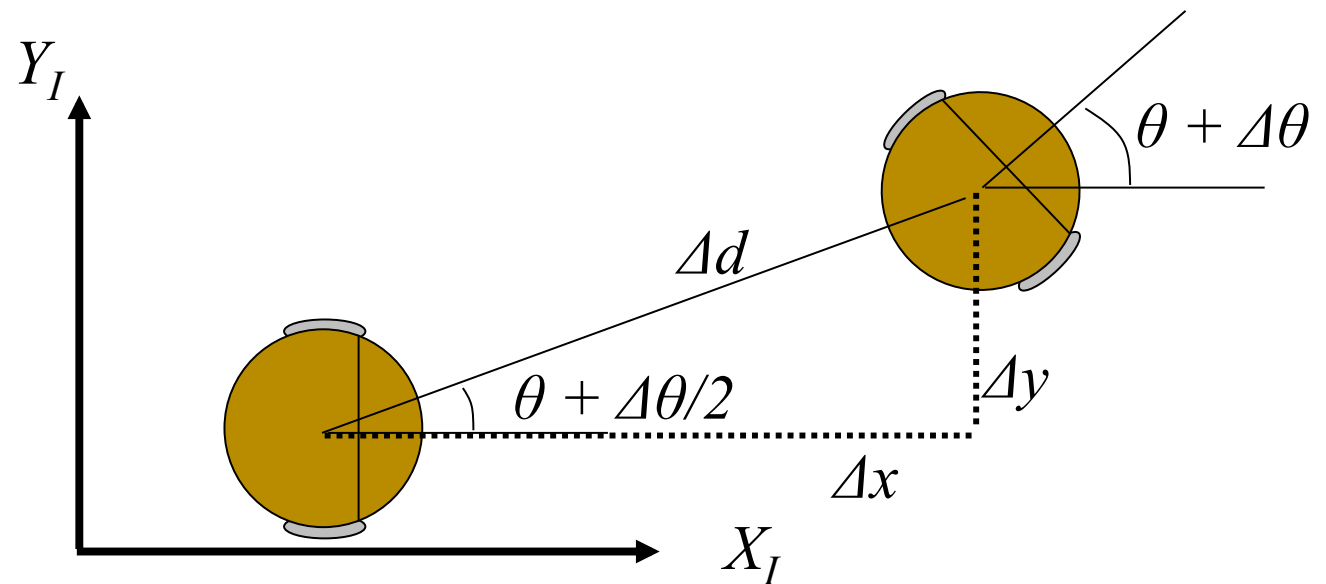
- Now that we have $\Delta\theta$ and Δs , we can calculate the position change in global coordinates.
 - We use a new segment of length Δd .





Modeling Motion

- Now calculate the change in position as a function of Δd .



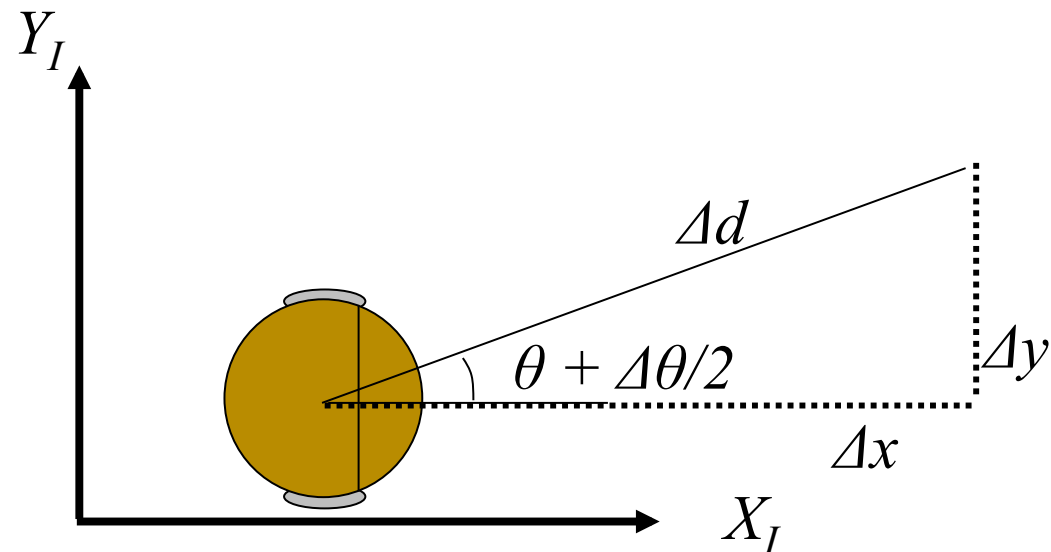


Modeling Motion

- Using Trig:

$$\Delta x = \Delta d \cos(\theta + \Delta\theta/2)$$

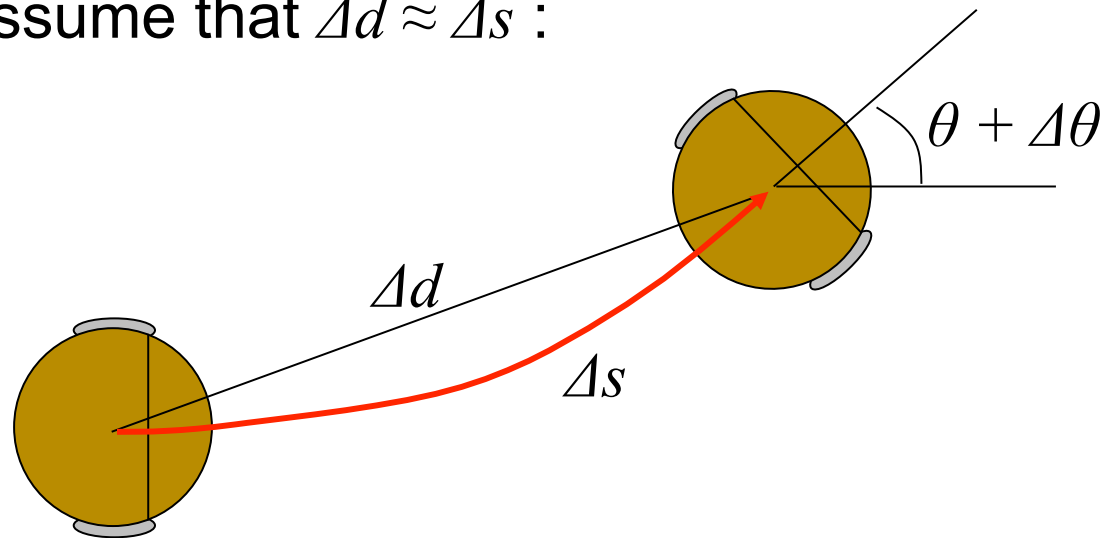
$$\Delta y = \Delta d \sin(\theta + \Delta\theta/2)$$





Modeling Motion

- Now if we assume that the motion is small, then we can assume that $\Delta d \approx \Delta s$:



- So...

$$\Delta x = \Delta s \cos(\theta + \Delta\theta/2)$$

$$\Delta y = \Delta s \sin(\theta + \Delta\theta/2)$$



Modeling Motion

- Summary:

$$\Delta x = \Delta s \cos(\theta + \Delta\theta/2)$$

$$\Delta y = \Delta s \sin(\theta + \Delta\theta/2)$$

$$\Delta\theta = \frac{\Delta s_r - \Delta s_l}{2L}$$

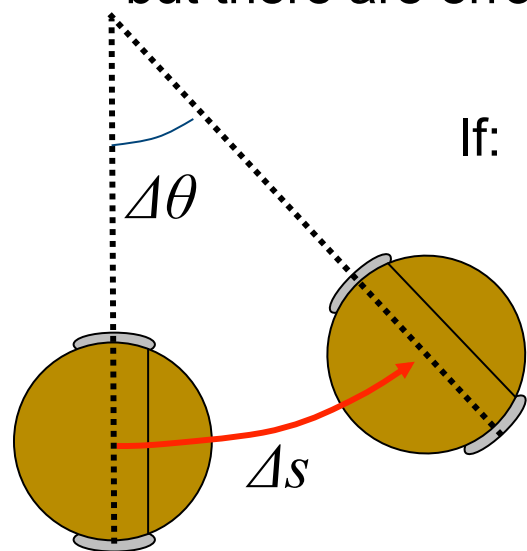
$$\Delta s = \frac{\Delta s_r + \Delta s_l}{2}$$

$$X_t = f(x, y, \theta, \Delta s_r, \Delta s_l) = \begin{bmatrix} x \\ y \\ \theta \end{bmatrix} + \begin{bmatrix} \frac{\Delta s_r + \Delta s_l}{2} \cos\left(\theta + \frac{\Delta s_r - \Delta s_l}{4L}\right) \\ \frac{\Delta s_r + \Delta s_l}{2} \sin\left(\theta + \frac{\Delta s_r - \Delta s_l}{4L}\right) \\ \frac{\Delta s_r - \Delta s_l}{2L} \end{bmatrix}$$



Modeling Uncertainty in Motion

- Let's consider wheel rotation measurement errors, and see how they propagate into positioning errors.
 - Example: the robot actually moved forward 1 m on the x axis, but there are errors in measuring this.



$$\Delta s = 1 + e_s$$

$$\Delta \theta = 0 + e_\theta$$

where e_s and e_θ are error terms



Modeling Uncertainty in Motion

- According to the following equations, the error $e_s = 0.001\text{m}$ produces errors in the direction of motion.

$$\Delta x = \Delta s \cos(\theta + \Delta\theta/2)$$

$$\Delta y = \Delta s \sin(\theta + \Delta\theta/2)$$

- However, the $\Delta\theta$ term affects each direction differently.
If $e_\theta = 2$ deg and $e_s = 0$ meters, then:

$$\cos(\theta + \Delta\theta/2) = 0.9998$$

$$\sin(\theta + \Delta\theta/2) = 0.0175$$



Modeling Uncertainty in Motion

- So

$$\Delta x = 0.9998$$

$$\Delta y = 0.0175$$

- But the robot actually went to $x = 1, y = 0$, so the errors in each direction are

$$\Delta x = +0.0002$$

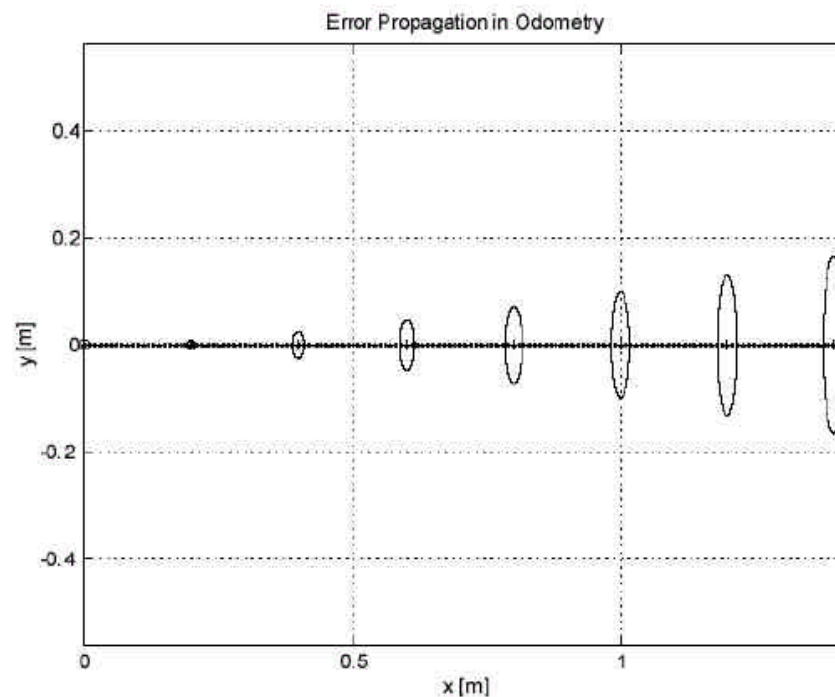
$$\Delta y = -0.0175$$

- ***THE ERROR IS BIGGER IN THE “Y” DIRECTION!***



Modeling Uncertainty in Motion

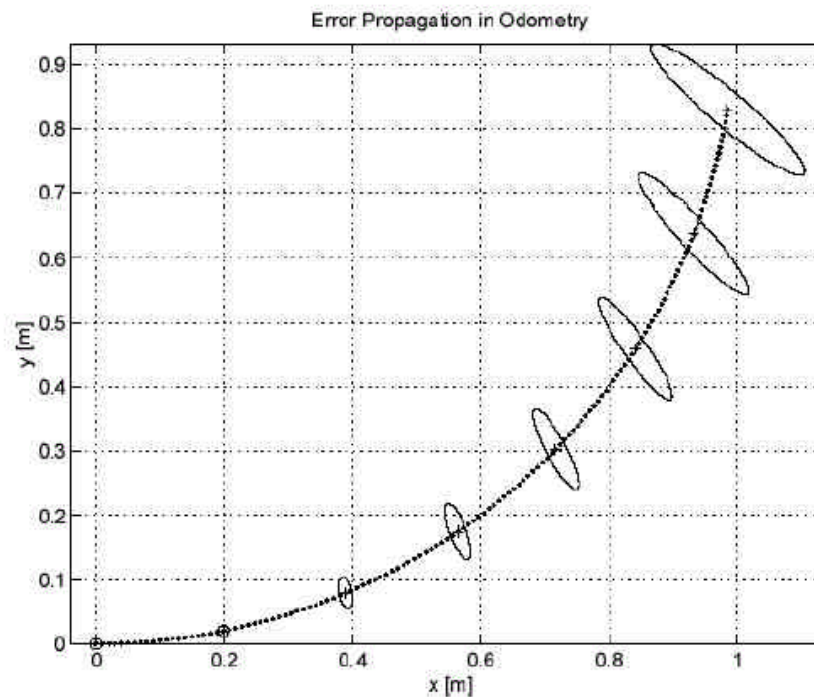
- Errors perpendicular to the direction grow much larger.





Modeling Uncertainty in Motion

- Error ellipse does not remain perpendicular to direction.





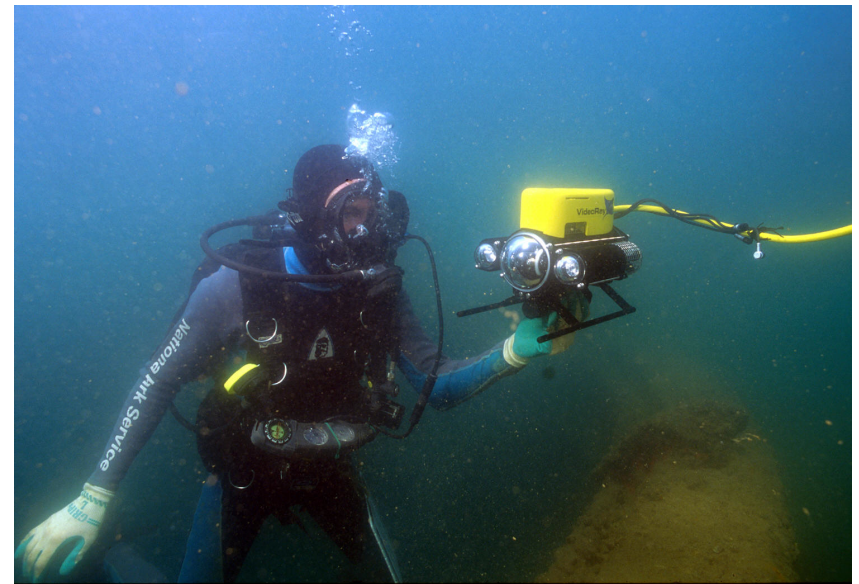
Odometry Kinematics

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The VideoRay MicroROV

- ROV Specs
 - Two horizontal thrusters, one vertical
 - Forward facing color camera
 - Rear facing B/W camera
 - 1.4 m/s (2.6 knots) speed
 - 152m depth rating
 - **Depth & Heading** sensors
 - SeaSprite Scanning **Sonar**





The VideoRay MicroROV

- ROV Modeling

$$\begin{aligned}m[\dot{u} - vr + wq - x_G(q^2 + r^2) + y_G(pq - \dot{r}) + z_G(pr + \dot{q})] &= X \\m[\dot{v} - wp + ur - y_G(r^2 + p^2) + z_G(qr - \dot{p}) + x_G(qp + \dot{r})] &= Y \\m[\dot{w} - uq + vp - z_G(p^2 + q^2) + x_G(rp - \dot{q}) + y_G(rq + \dot{p})] &= Z \\I_x \dot{p} + (I_z - I_y)qr - (\dot{r} + pq)I_{xz} + (r^2 - q^2)I_{yz} + (pr - \dot{q})I_{xy} \\+ m[y_G(\dot{w} - uq + vp) - z_G(\dot{v} - wp + ur)] &= K \\I_y \dot{q} + (I_x - I_z)rp - (\dot{p} + qr)I_{xy} + (p^2 - r^2)I_{zx} + (qp - \dot{r})I_{yz} \\+ m[z_G(\dot{u} - vr + wq) - x_G(\dot{w} - uq + vp)] &= M \\I_z \dot{r} + (I_y - I_x)pq - (\dot{q} + rp)I_{yz} + (q^2 - p^2)I_{xy} + (rq - \dot{p})I_{zx} \\+ m[x_G(\dot{v} - wp + ur) - y_G(\dot{u} - vr + wq)] &= N\end{aligned}$$

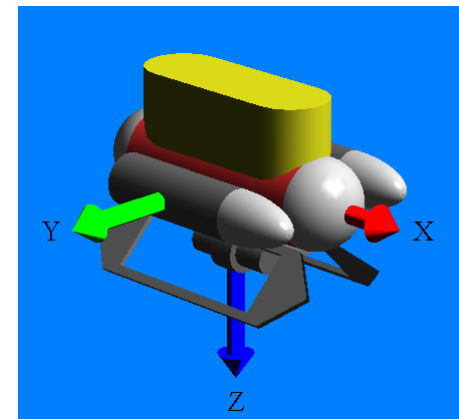


Equations of Motion

- 6 degrees of freedom (DOF):
- State vectors:
body-fixed velocity vector:
earth-fixed pos. vector:

$$\mathbf{v} = \begin{bmatrix} \mathbf{v}_1^T \\ \mathbf{v}_2^T \end{bmatrix} = [u, v, w, p, q, r]$$

$$\boldsymbol{\eta} = \begin{bmatrix} \boldsymbol{\eta}_1^T \\ \boldsymbol{\eta}_2^T \end{bmatrix} = [x, y, z, \phi, \theta, \psi]$$



DOF	Surge	Sway	Heave	Roll	Pitch	Yaw
Velocities	u	v	w	p	q	r
Position & Attitude	x	y	z	ϕ	θ	ψ
Forces & Moments	X	Y	Z	K	M	N



Equations of Motion

- Initial Assumptions
 - The ROV will usually move with low velocity when on mission
 - Almost three planes of symmetry;
 - Vehicle is assumed to be performing non-coupled motions.



Equations of Motion

- Horizontal Plane:

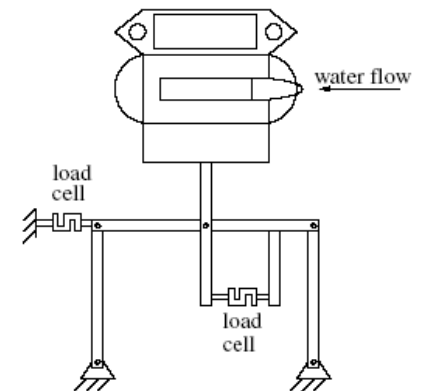
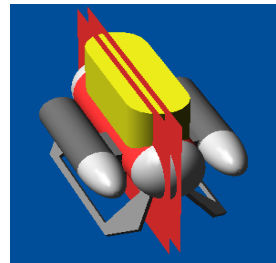
$$\begin{aligned}m_{11}\dot{u} &= -m_{22}vr + X_u u + X_{u|u}|u| + X \\m_{22}\dot{v} &= m_{11}ur + Y_v v + Y_{v|v}|v|, \\I\dot{r} &= N_r r + N_{r|r}|r| + N,\end{aligned}$$

- Vertical Plan:

$$m_{33}\dot{w} = Z_w w + Z_{w|w}|w| + Z$$

Theory vs. Experiment

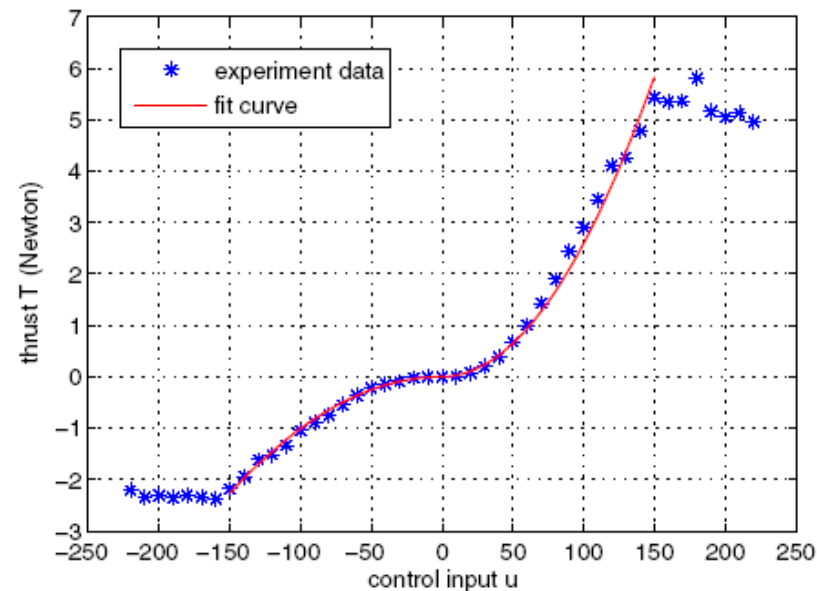
- Coefficients for the dynamic model are pre-calculated using strip theory;
- A series of tests are carried out to validate the hydrodynamic coefficients, including
 - Propeller mapping
 - Added mass coefficients
 - Damping coefficients





Propeller Thrust Mapping

- The forward thrust can be represented as:

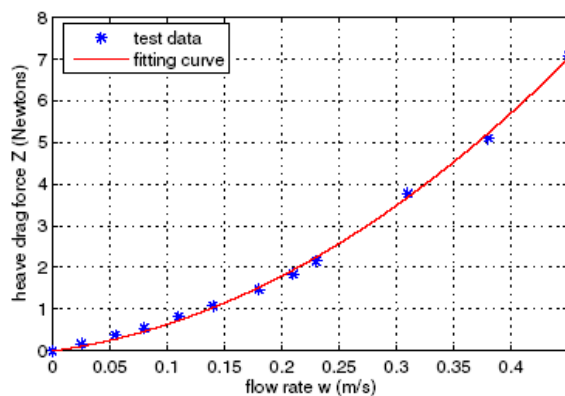




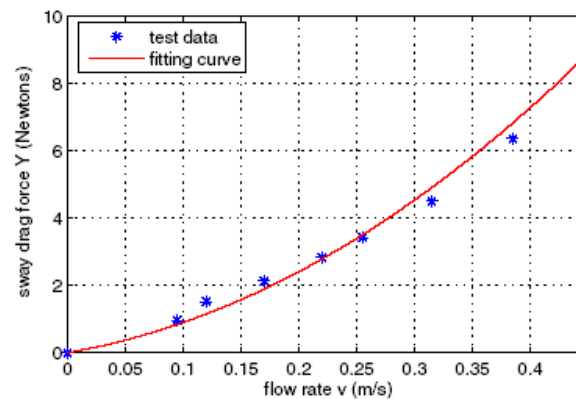
Direct Drag Forces

- The drag can be modeled as non linear functions

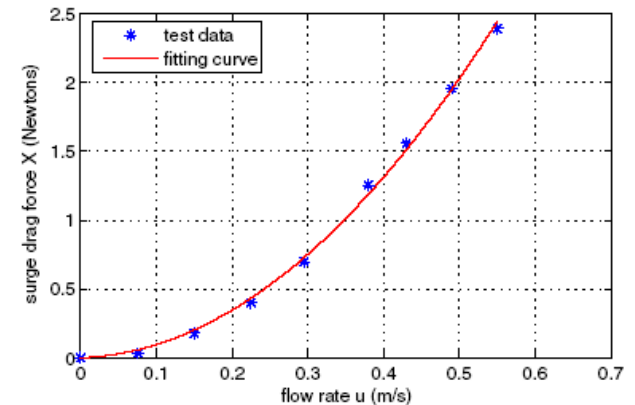
Drag in Heave (Z)
Direction



Drag in Sway (Y)
Direction



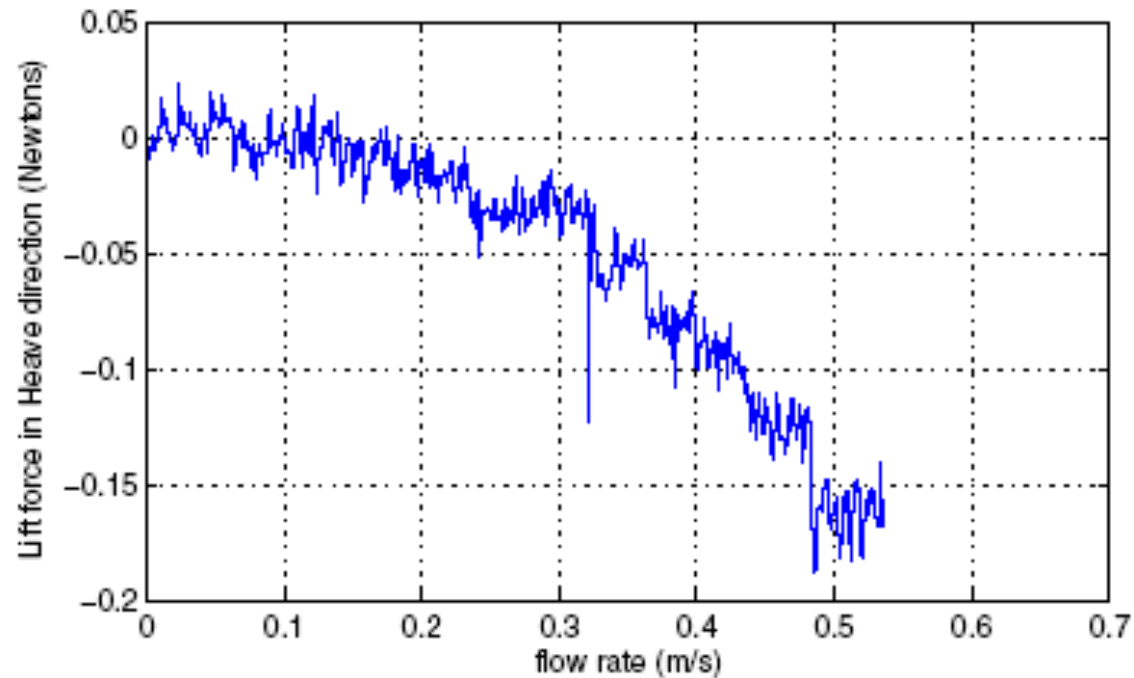
Drag in Surge (X)
Direction





Perpendicular Drag Forces

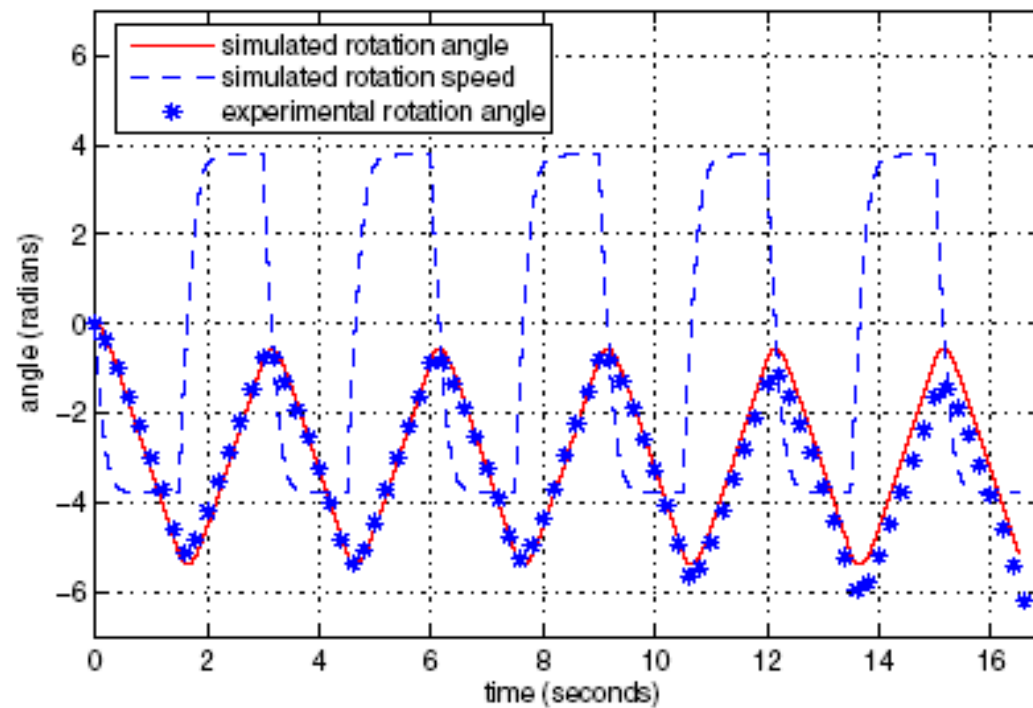
- Heave (Z) drag from surge speed





Model Verification

- Yaw Verification





Model Verification

- Surge Verification

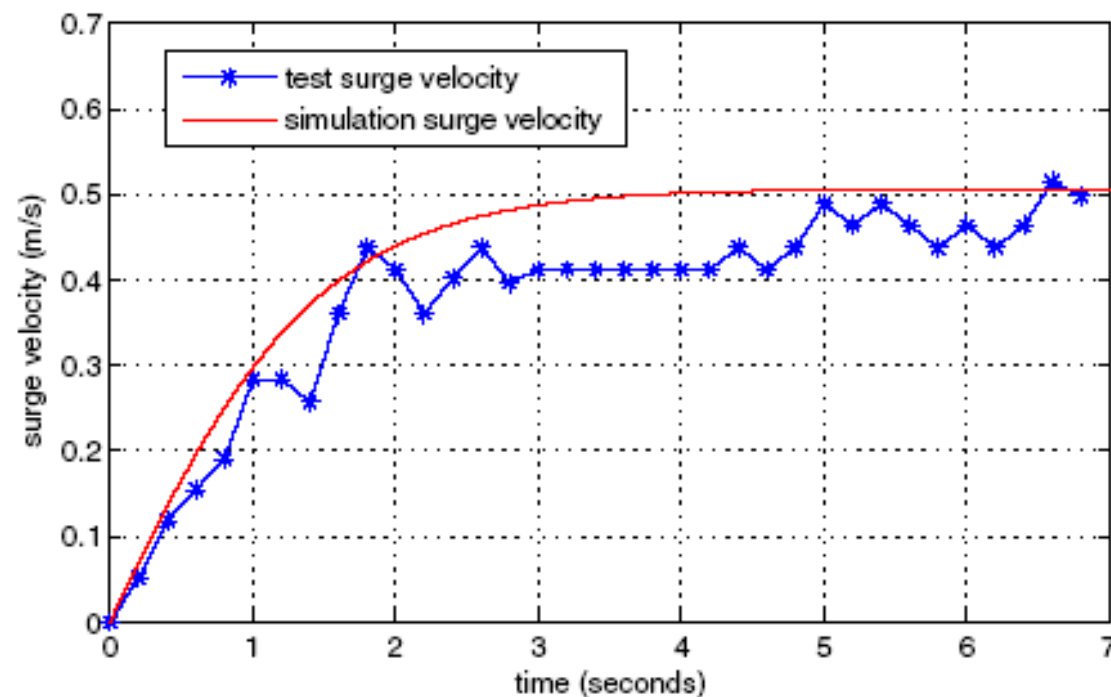
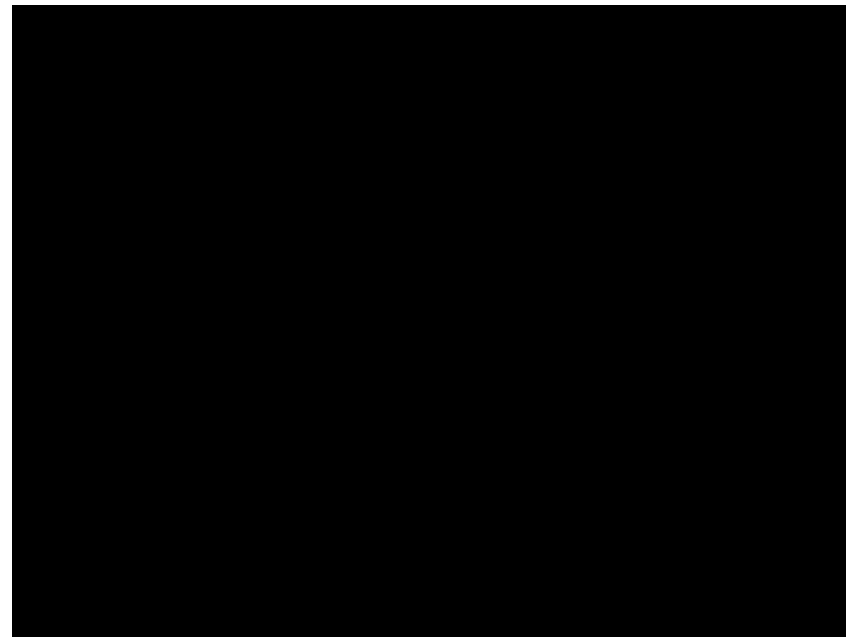


Fig. 14. Surge test experiment data and simulation result



Autonomous Control





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Odometry on the Jaguar

- Goals:
 - Calculate the resulting robot position and orientation from wheel encoder measurements.
 - Display them with the Matlab plot function



Odometry on the Jaguar

- Method cont':
 - Make use of the fact that your encoder has resolution of 4096 pulses per revolution. Be able to convert this to a distance travelled by the wheel.

$$r\varphi_r = \Delta s_r$$

- Given the distance travelled by each wheel, we can calculate the change in the robot's distance and orientation.

$$\Delta s = \frac{\Delta s_r + \Delta s_l}{2} \qquad \Delta \theta = \frac{(\Delta s_r - \Delta s_l)}{2L}$$



Odometry on the Jaguar

- Method cont':
 - Now you should be able to update the position/ orientation in global coordinates.

$$\Delta x = \Delta s \cos(\theta + \Delta\theta/2)$$

$$\Delta y = \Delta s \sin(\theta + \Delta\theta/2)$$